



4V-60V Input Current Mode Synchronous Boost Controller

DESCRIPTION

The VE8602 is a high-voltage, synchronous, step-up controller. The VE8602 uses current mode control with cycle-by-cycle peak current limiting or hiccup mode OCP.

The VE8602 has DEM (diode emulation mode) that optimizes light-load efficiency.

The operating frequency of the VE8602 can be programmed by an external resistor or synchronized to an external clock from 100kHz to 1MHz.

The VE8602 offers programmable soft-start and power-good indicator. Full protection features include precision output over-voltage protection (OVP), output over-current protection (OCP), and thermal shutdown.

The VE8602 offers shunt and DCR current sensing. DCR sensing provides higher efficiency but lower current limit accuracy.

The VE8602 is available in TSSOP20-EP and QFN-20 (3mm x 4mm Wettable Flank) packages. Both packages use EPAD to improve thermal performance and noise immunity. Low pin count, fewer external components, and default internal values make VE8602 an ideal solution for time to market simple power supply design.

Automotive-compliant parts are available under separate datasheet (VE8602Q).

FEATURES

- Wide 4V to 60V Operating Input Range
- Dual N-Channel MOSFET Driver
- 0.8V Voltage Reference with ±1.5% Accuracy
 Over Temperature
- Programmable Frequency Range: 100kHz-1MHz
- Quasi-Bypass Operation
- External Sync Clock Range: 100kHz-1MHz
- 180º Out-of-Phase SYNCO Pin and Dither
- Programmable Soft Start (SS)
- Power Good (PG) Output Voltage Monitor
- Selectable Cycle-by-Cycle Current Limit
- Output Over-Voltage Protection (OVP)
- Hiccup Mode Over-Current Protection
- Internal LDO with External Power Supply
 Option
- Programmable CCM and DEM Mode
- Available in TSSOP20-EP and QFN-20 (3mm x 4mm Wettable Flank) Packages

APPLICATIONS

- Audio Power Supply
- Industrial
- High Current Boost Power Supply



TYPICAL APPLICATION



V_{IN} > 5.5V DCR Sensing Application



4V < VIN-MIN < 5.5V DCR Sensing Application





VIN-MIN < 4V DCR Sensing Application



BLOCK DIAGRAM



ORDERING INFORMATION

Part Number	Part Marking	Package	Packing Type	Temp Range
VE8602A5R	8602	TSSOP20-EP	Tape and Reel / Detail in page 25	-40 to +125°C
VE8602AKR	8602	QFN-20	Tape and Reel / Detail in page 25	-40 to +125°C



PIN CONFIGURATIONS



PIN DESCRIPTION

Name	TSSOP20- EP	QFN-20	Description
VIN	1	10	Input supply. This pin should be tied to input rail. Decouple this
VIIN	I	13	pin with a small ceramic capacitor to ground.
			Enable input. The threshold is 1.2V with 120mV of hysteresis and
			is used to implement an input under-voltage lockout (UVLO)
EN/SYNC	2	20	function externally. If an external sync clock (the frequency is
			higher than default frequency set by FREQ) is applied to
		2	EN/SYNC, the internal clock follows the sync frequency.
			External power supply for the internal VCC regulator. EXTBIAS
			disables the power from VIN for as long as EXTBIAS is higher than
EXTBIAS	3	1	4.7V. Do not connect a power supply greater than 24V to EXTBIAS.
			Connect EXTBIAS to an external power supply to reduce power
C			dissipation and increase efficiency.
VCC	1	2	Internal bias supply. 5V internal bias supply. A ≥4.7µF decoupling
VCC	4	2	capacitor is required between VCC and PGND.
SCND	F	2	Low-noise ground reference. SGND should be connected to the
SGIND	5	3	ground side of the output capacitors.
22	6	1	Soft-start control input. SS is used to program the soft-start
	0	4	period with an external capacitor between SS and SGND.
			Regulation control loop compensation. Connect an RC network
COMP	7	5	from COMP to SGND to compensate for the regulation control
			loop.



Name	TSSOP20- EP	QFN-20	Description
FB	8	6	Feedback. Connect FB to a resistor voltage divider from the output to ground.
CCM/DEM	9	7	Continuous conduction mode/Diode emulation mode (DEM). Floating CCM/DEM or connecting CCM/DEM to VCC makes the part operate in CCM. Connecting an appropriate external resistor from CCM/DEM to SGND makes the part operate in DEM mode. The DEM voltage should be no less than 300mV
FREQ	10	8	Frequency. Connect a resistor between FREQ and SGND to set the switching frequency.
PG	11	9	Power good output. The output of PG is an open drain.
ILIM	12	10	Sense voltage limit set. The voltage at ILIM sets the nominal sense voltage at the maximum output current. There are three fixed options: float, VCC, and SGND. Connect a resistor or a voltage source that is higher than 0.64V and lower than 1.5V to disable the hiccup mode.
SYNCO/ DITHER	13	11	Frequency synchronous out. SYNCO outputs a 180° out-of- phase clock when the part works in CCM for dual-channel operation. Connect to GND to enable the dither.
SENSE-	14	12	Negative input for the current sense. The sensed inductor current limit threshold is determined by the status of ILIM.
SENSE+	15	13	Positive input for the current sense. The sensed inductor current limit threshold is determined by the status of ILIM.
PGND	16	14	Power ground. Connect PGND directly to the negative terminal of the VCC decoupling capacitor.
BG	17	15	Bottom gate driver output. Connect BG to the gate of the bottom MOSFET.
SW	18	16	Switch node. SW is the reference for the V_{BST} supply and high- current returns for the bootstrapped switch.
TG	19	17	Top gate drive. TG drives the gate of the top MOSFET. The TG driver draws power from the BST capacitor and returns to SW, providing a true floating drive to the top N-channel MOSFET.
BST	20	18	Bootstrap. BST is the positive power supply for the high-side MOSFET driver. Connect a bypass capacitor between BST and SW. A Schottky or high-speed diode must be tied from VCC to BST.
EPAD			Exposed pad. The exposed pad is on the bottom side of device. It is not electrically connected to SGND or PGND. Connect the exposed pad to SGND and PGND during PCB layout for better thermal performance.

ABSOLUTE MAXIMUM RATINGS

Parameter	Minimum	Maximum	Unit
VIN	-0.3	+65	V
SW	-0.3	+65	V
SW (transient < 20 ns)	-5	+65	V
BST to SW	-0.3	VCC+0.3	V
TG to SW	-0.3	VCC+0.3	V
EN/SYNC	-0.3	+65	V
VCC	-0.3	+6.5	V
EXTBIAS	-0.3	+26	V
SENSE+-	-0.3	+65	V
SENSE+ to SENSE-	-0.3	+0.3	V
All Other Pins	-0.3	VCC+0.3	V
Junction Temperature		+150	°C

ESD RATINGS

Parameter	(Value	Unit				
Human Body Model (HBM)		2	kV				
Charged Device Model (CDM)	$\langle \rangle$	1	kV				
Latch-Up		100	mA				

THERMAL INFORMATION

Thermal Resistance	θ _{JA} (°C/W)	θ _{JC} (°C/W)
TSSOP20-EP	40	8
QFN-20	48	10

RECOMMENDED OPERATINIG CONDITIONS

Parameter	Minimum	Maximum	Unit
Temperature	-40	+125	°C
VIN to GND	+4	+60	V
EN / SYNC	0	+60	V
SENSE+,SENSE- to GND	0	+60	V
EXTBIAS to GND	+4.7	+24	V

ELECTRICAL CHARACTERISTICS

 $V_{IN} = 24V$, $V_{EN} = 2V$, $V_{EXTBIAS} = 0V$, $V_{ILIM} = Floating$, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Unit
Input Supply						
VIN UVLO threshold (rising)	VIN_UV_RISING			4.08		V
VIN UVLO threshold (falling)	VIN_UV_FALLING			3.78		V
V _{IN} UVLO hysteresis	VIN_UV_HYS			300		mV
V _{IN} supply current with EXTBIAS bias	I _{Q_EXTBIAS}	EXTBIAS = 12V, no switching, $V_{CCM/DEM} = 5V$, $V_{FB} = 0.84V$, SENSE+ = SENSE- = 0V		8	A	μΑ
V _{IN} supply current without EXTBIAS bias	la	EXTBIAS = 0V, no switching, $V_{CCM/DEM} = 5V, V_{FB} = 0.84V,$ SENSE+ = SENSE- = 0V		1570		μA
V _{IN} DEM current	Iq_dem	EXTBIAS = 0V, no switching, $V_{CCM/DEM} = 0.6V$, $V_{FB} = 0.84V$, SENSE+ = SENSE- = 12V		436		μΑ
VIN shutdown current	ISHDN	$V_{EN} = 0V$		4	15	μA
VCC Regulator						
VCC regulator output voltage from V _{IN}	VCC _{VIN}	$V_{IN} > 6V$, $I_{LOAD} = 0$ to 50mA	4.75	5	5.25	V
VCC regulator load regulation from V _{IN}		$I_{LOAD} = 0$ to 50mA, EXTBIAS floating or connected to SGND		2	5	%
VCC regulator output voltage from EXTBIAS	VCCextbias	EXTBIAS > 6V	4.75	5	5.25	V
VCC regulator load regulation from EXTBIAS	8-V	I _{LOAD} = 0 to 50mA, EXTBIAS = 12V		1	3	%
EXTBIAS UVLO threshold (rising)	EXTBIAS_ RISING		4.3	4.68	4.92	V
EXTBIAS UVLO threshold (falling)	EXTBIAS_ FALLING		4.05	4.42	4.75	V
EXTBIAS threshold hysteresis	EXTBIAS_ HYS			258	278	mV
		$V_{DEM} = 5V, V_{FB} = 0.84V,$ SENSE+ = SENSE- = 12V, EXTBIAS = 12V, no switching		960		μA
EX I BIAS supply current	IEXTBIAS	$V_{DEM} = 0.6V, V_{FB} = 0.84V,$ SENSE+ = SENSE- = 12V, EXTBIAS = 12V, no switching		500		μA
Feedback (FB)						
Feedback voltage	V _{FB}	4V < V _{IN} < 60V	0.788	0.8	0.812	V



Parameter	Symbol	Condition	Min	Тур	Max	Unit			
Feedback current	I _{FB}	$V_{FB} = 0.8V$		10		nA			
Enable (EN/SYNC)									
Enable threshold (rising)	Ven_rising			1.2	1.25	V			
Enable threshold (falling)	Ven_falling			1.08		V			
Enable threshold hysteresis	Ven_th			120		mV			
Enable input current	I _{EN}	$V_{EN} = 2V$		1	2	μA			
Enable turn-off delay	T _{OFF}		18	42	72	μs			
Oscillator and Sync				X					
Operating frequency	Fsw	$R_{FREQ} = 90k\Omega$		500		kHz			
Foldback operating frequency	Fsw_foldback	V _{FB} = 0.1V		50%		Fsw			
Maximum frequency	Fswн		1000			kHz			
Minimum frequency	FswL				100	kHz			
EN/SYNC frequency range	FSYNC		100		1000	kHz			
EN/SYNC voltage rising threshold	VSYNC_RISING		2			V			
EN/SYNC voltage falling threshold	VSYNC_FALLING	0			0.35	V			
Current Sense									
Current sense common mode voltage range	Vsense+/-		0		65	V			
		ILIM = SGND, V _{SENSE+} = 12V	14	24	34				
Current limit sense voltage	VILIMIT	ILIM = VCC, V _{SENSE+} = 12V	39	49	59	mV			
		ILIM = FLOAT, V _{SENSE+} = 12V	64	74	84				
		ILIM = SGND, $V_{SENSE+} = 12V$		8					
Reverse current limit sense	VREV_ILIMIT	ILIM = VCC, V _{SENSE+} = 12V		16		mV			
voltage		ILIM = FLOAT, V _{SENSE+} = 12V		25					
	lanuar	$V_{SENSE+} = V_{SENSE-} = 12V$	240	270	300	μA			
Input surrent of sensor	ISENSE+	VSENSE+ = VSENSE- = 1V			1				
input current of sensor		V _{SENSE+} = V _{SENSE-} = 12V			1				
7	ISENSE-	VSENSE+ = VSENSE- = 1V			1	μΑ			
Soft Start (SS)									
Soft-start source current	lss	SS = 0.5V	2	4	6	μA			
Error Amplifier (EA)									
Error amp transconductance	Gм	$\Delta V = 5 m V$	360	550	750	μS			



Parameter	Symbol	Condition	Min	Тур	Max	Unit
Error amp open loop DC	Ao		70	75	82	dB
gain	,		10	10	02	u.D
Error amp sink/source	FA	FB = 0.7/0.9V		±50		uА
current						I.
Protection						
Over-voltage threshold	Vov		110%	116%	120%	VFB
Over-voltage hysteresis	V _{OV_HYS}			3%		V _{FB}
Thermal shutdown				170		°C
Thermal shutdown				20		°C
hysteresis				20	P	Ŭ
Gate Driver						
TG pull-up resistor	Rtg_pullup		\sim	2		Ω
TG pull-down resistor	RTG_PULLDN			1		Ω
BG pull-up resistor	R _{BG_PULLUP}			2		Ω
BG pull-down resistor	Rbg_pulldn			1		Ω
Dead time	TDEAD			20		ns
TG minimum on time	Ton_min_tg			170		ns
BG minimum on time	TON_MIN_BG			145		ns
Power Good (PG)						
Power good low	V _{PG_LOW}	I _{LOAD} = 4mA		0.2	0.3	V
DC riging threshold		Vout rising		90%		VFB
	F GVTH_RSING	Vout falling		110%		VFB
PC falling throshold		Vout falling		88%		VFB
	F GVIH_FALLING	Vout rising		112%		VFB
PG threshold hysteresis	PG _{VTH_HYS}			2%		V _{FB}
Power good leakage	IPG_LK	PG = 5V			2	μA
Dewer good delay	т	Rising		70		
Fower good delay	I PG_DELAY	Falling		55	μs	
DEM Mode/CCM						
DEM mode output current	IDEM	R _{FREQ} = 90 kΩ		6.5		μA
CCM required DEM	Voorentie		2			V
threshold voltage	V CCM_TH		3			v

 $V_{IN} = 24V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$, unless otherwise noted.



 $V_{IN} = 24V$, $T_J = -40^{\circ}C$ to +125°C, unless otherwise noted.



 $V_{IN} = 24V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$, unless otherwise noted.



 V_{IN} = 12V, V_{OUT} = 25V, T_J = -40°C to +125°C, unless otherwise noted.



 V_{IN} = 12V, V_{OUT} = 25V, T_J = -40°C to +125°C, unless otherwise noted.



FUNCTION DESCRIPTION

General Description

The VE8602 is a high-performance, step-up, synchronous, DC/DC controller IC with a wide input voltage range. It implements current mode control and an internal slope compensation to avoid the subharmonic oscillation.

Diode Emulation Mode

The VE8602 offers diode emulation mode (DEM) functionality to optimize efficiency during light load. DEM is enabled when CCM/DEM is at a low level by connecting an appropriate resistor (Rccm/DEM) to SGND.

The recommended value for RCCM/DEM is

0.5R_{FREQ} <RCCM/DEM<1.5R_{FREQ}

The value less than 0.5R_{FREQ} is not allowed but the value higher than 1.5R_{FREQ} and less than 3R_{FREQ} is allowed. The higher value of R_{CCM/DEM} increases output voltage ripple but reduces the power loss during light load.

Gate Driver

The low-side gate driver is supplied from VCC. The high-side gate driver is supplied from BST. A boot capacitor connected from the BST to the VCC provides power to the high-side MOSFET driver. This floating driver has its own under-voltage lockout (UVLO) protection. This UVLO's rising threshold is 3.6V with a hysteresis of 100mV. If the BST voltage is lower than the bootstrap UVLO, the VE8602 enters boot refresh mode to ensure that the BST capacitor is high enough to drive the HS-FET.

Error Amplifier

The error amplifier compares V_{FB} with the internal 0.8V reference and outputs a current proportional to the difference between the two input voltages. This output current is then used to charge or discharge the external compensation network to form V_{COMP} , which is used to control the inductor current. Adjusting the compensation network from COMP to SGND optimizes the control loop for good stability or fast transient response.

Current Limit Function

There are three fixed current limit options: 23mV, when ILIM is connected to SGND; 48mV, when ILIM is connected to VCC; and 74mV, when ILIM is floating.

When the peak value of the inductor current exceeds the set current-limit threshold, the output voltage begins dropping until FB is 37.5% below the reference. The VE8602 enters hiccup mode to restart the part periodically. All switchers are turned off for 28ms before a re-start up is issued. The frequency is lowered when FB is below 0.4V. This protection mode is especially useful when the output is dead- shorted to ground. The average short-circuit current is reduced greatly to alleviate thermal issues. The VE8602 exits hiccup mode once the over-current condition is removed.

The VE8602 works on peak current limit mode and the hiccup mode is disabled when the voltage on the ILIM is between 0.64V and 1.5V before soft start. The current limit threshold can be calculated by Equation (1):

$$I_{\text{LIM}} = \frac{V_{\text{ILIM}} - 0.64}{10 \times R_{\text{s}}} \qquad (1)$$



Power Good

The VE8602 includes an open-drain power good output that indicates whether the regulator's output is within $\pm 10\%$ of its nominal value. When the output voltage falls outside of this range, the PG output is pulled low. PG should be connected to a voltage source no more than 5V through a resistor (e.g.: $100k\Omega$).

Soft Start (SS)

Soft start (SS) is implemented to prevent the converter output voltage from overshooting during start-up. When the chip starts up, the internal circuitry generates a soft-start voltage that ramps up from 0V to 2.8V. When it is lower than REF, SS overrides REF, so the error amplifier uses SS as the reference. When SS is higher than REF, REF regains control.

An external capacitor connected from SS to SGND is charged from an internal 4μ A current source, producing a ramped voltage. The soft - start time (T_{SS}) is set by the external SS capacitor and can be calculated by Equation (2):

(2)

$$\Gamma_{SS}(ms) = \frac{C_{SS}(nF) \times V_{REF}(V)}{I_{SS}(uA)}$$

Where C_{SS} is the external SS capacitor, V_{REF} is the internal reference voltage (0.8V), and I_{SS} is the 4µA SS charge current. There is no internal SS capacitor. SS is reset when a fault protection other than OVP or peak current limit occurs.

Programmable Switching Frequency

The VE8602's frequency can be programmed from 100KHz to 1000KHz with a resistor from FREQ to SGND. The Value of R_{FREQ} can be calculated with Equation (3):

$$R_{FREQ}(K\Omega) = \frac{1000}{0.0202 \times F_{SW}(KHz)} - 9$$
 (3)

OVP

The output over-voltage is monitored by V_{FB}. If V_{FB} is typically 16% higher than the reference, the VE8602 enters tri-state mode. The HS-FET and LS-FET turn off. The VE8602 works in tri-state mode until the over-voltage condition is cleared.

EN/SYNC

The VE8602 has a dedicated enable (EN/SYNC) control that uses a bandgap - generated precision threshold of 1.2V. By pulling EN/SYNC high or low, the IC can be enabled or disabled. To disable the part, EN/SYNC must be pulled low for at least 42µs. The internal clock rising edge is synchronized to the external clock rising edge. The pulse width (both high and low) of the external clock signal should be no less than 100ns. The frequency applied on EN/SYNC pin of external clock must be higher than the frequency set by FREQ pin.

SYNCO Function

The SYNCO pin outputs a default 180° phase shifted clock when VE8602 works in CCM. This function allows two devices operate in same frequency but 180°out of phase to reduce the total input current ripple, so that a smaller input bypass capacitor can be used.



Dithering Function

If VE8602 is set to CCM. It works on dithering mode when the SYNCO pin is shorted to GND before start up.

UVLO

Under-voltage lockout (UVLO) is implemented to protect the chip from operating at an insufficient input supply voltage. The VE8602 UVLO rising threshold is about 4.1V, while its falling threshold is a consistent 3.8V.

Thermal Protection

Thermal protection prevents damage to the IC from excessive temperature. The die temperature is monitored internally until the thermal limit is reached. When the silicon die temperature is higher than 170°C, the entire chip shuts down. When the temperature is lower than its lower threshold (typically 150°C), the chip is enabled again.

Start-Up and Shutdown

If both V_{IN} and EN/SYNC are higher than their respective thresholds, the chip starts up. The reference block starts first, generating stable reference voltages and currents. The internal regulator is then enabled. The regulator provides a stable supply for the remaining circuitry. Three events can shut down the chip: EN low, V_{IN} low, and thermal shutdown. During the shutdown procedure, the signal path is blocked first to avoid any fault triggering. V_{COMP} and the internal supply rail are then pulled down.

Pre-Bias Start-Up

If SS is less than FB at start-up, and the output has a pre-bias voltage, neither TG nor BG is turned on until SS is greater than FB.

VCC Regulator Connection

VCC can be powered from both VIN and EXTBIAS. If connecting EXTBIAS to an external power supply, EXTBIAS should be higher than 4.7V but less than 24V. When V_{IN} is less than 5.5V, EXTBIAS should be biased by external source. If V_{OUT} is higher than 5V but less than 24V, EXTBIAS can be connected to V_{OUT} with a resistor or diode. The recommend value of this resistor is 10Ω .



Figure 29. VCC Regulator Connection

Quasi-Bypass operation

The VE8602 allows >99.9% duty cycle operation for the high side MOSFET when the input voltage is equal to or greater than the target output voltage.



APPLICATION

Setting the Output Voltage

The external resistor divider is used to set the output voltage (see Figure 30.)



Figure 30. Setting the Output Voltage

If R8 is known, then R9 can be calculated with Equation (4):

$$R9 = R8 \div (\frac{V_{OUT}}{0.8V} - 1) \quad (4)$$

Setting Current Limit

The VE8602 has three fixed current limit options: 23mV (V_{SENSE+} - V_{SENSE-}), when ILIM is connected to SGND; 48mV, when ILIM is connected to VCC; and 74mV, when ILIM is floating. Ensure that the application can deliver a full load of current over the full operating temperature range when setting ILIM.

The current sense resistor (R_{SENSE}) monitors the inductor current. Its value is chosen based on the current limit threshold. The relationship between the peak inductor current (I_{PK}) and R_{SENSE} can be calculated with Equation (5):

$$R_{SENSE} = \frac{V_{ILIMIT}}{I_{PK}} \quad (5)$$

The VE8602 works on peak current limit mode and the hiccup mode is disabled when the voltage on the ILIM is between 0.64V and 1.5V before soft start. The current limit threshold can be calculated by Equation (1). The VE8602 integrates a 5uA current source and a 500k Ω resistor. The Voltage on the ILIM pin is 2.5V when this pin is floating.



Figure 31. ILIM Internal Circuit



Slope Compensation

An internal slope compensation is designed to avoid the subharmonic issue. The value of this slope is 400mV when the duty cycle is maximum. To avoid the subharmonic issue the inductor L can be calculated with Equation (6):

$$L > \frac{(V_{OUT} - V_{IN}) \times 12 \times R_{SENSE}}{0.8 \times F_{SW}} \quad (6)$$

where F_{SW} is the switching frequency.

BST Charge Diode and Resistor Selection

The recommended external BST diode is a Schottky diode. The recommended BST capacitor value is 0.1μ F to 1μ F and it must be less than 1/10 C_{VCC}. A resistor in series with the BST capacitor (R_{BST}) can reduce the TG rising rate and voltage spikes. This also helps adjust the deadtime. A resistor in series with BG helps enhance EMI performance and reduce voltage stress at a high V_{IN}.

DCR Sensing

For the applications requiring low cost with low power loss, DCR is used to sense the inductor current rather than using a sense resistor. Shown in figure 32. is a DCR sensing configuration.



R and C selection should meet Equation (7) since this indirect current sensing method requires a time constant matching. R is usually selected to be in the range of $1k\Omega$ to $10k\Omega$ and C can be calculated with Equation (7):

$$C = \frac{L}{DCR \times R} \qquad (7)$$

Switching Frequency

Switching frequency selection is a trade-off between efficiency and component size. Low switching frequency improves efficiency by reducing MOSFET switching loss. To meet the output ripple and load transient requirements, operation at a low switching frequency requires larger inductance and output capacitance. The switching frequency of the VE8602 is set by a resistor connected from the FREQ pin to GND according to Equation (3). In noise-sensitive applications, the switching frequency should be out of a sensitive frequency band.

Selecting the Inductor

An inductor with a DC current rating at least 20% higher than the maximum load current is recommended for most applications. A larger value inductor results in less ripple current and a lower output ripple voltage.



However, the larger value inductor has a larger size, higher series resistance, and lower saturation current. Choose the inductor ripple current to be approximately 20%~50% of the maximum input current. The inductance values can be calculated with Equation (8):

$$L = \frac{V_{IN}}{\Delta I_L \times F_{SW}} \left(1 - \frac{V_{IN}}{V_{OUT}}\right)$$
(8)

Selecting the Output Capacitor

The output capacitor is used to hold output voltage and suppress the output voltage ripple. The output voltage ripple can be estimated with Equation (9):

$$V_{\text{RIPPLE}} = \frac{I_{\text{OUT}} \times V_{\text{OUT}}}{V_{\text{IN}} \text{MIN}} \left(R_{\text{ESR}} + \frac{1}{4 \times C_{\text{OUT}} \times F_{\text{SW}}} \right) \quad (9)$$

Power MOSFET Selection

Two N-channel MOSFETs must be selected for the controller: one for the high-side switch, and one for the lowside switch. The driver level of the high-side and low-side MOSFETs is 5V, the logic level MOSFET is recommend.

PCB Layout Guidelines

Efficient PCB layout is critical to achieve good regulation, ripple rejection, transient response, and thermal performance. It is highly recommended to duplicate the EVB layout for optimum performance. If changes are necessary, refer to below figures and follow the guidelines below:

1. A four-layer layout is strongly recommended to achieve better thermal performance.

2. Place output bypass ceramic capacitors close to MOSFETs. Place the MOSFETs as close as possible to the ceramic capacitors.

3. Place the feedback resistors close to the chip to ensure that the trace which connects to FB is as short as possible. Route SW and BST away from sensitive analog areas such as FB, SENSE+ and SENSE - .

4. Use a large ground plane to connect to PGND directly. Add vias near PGND if the bottom layer is a ground plane. Use multiple vias to connect the power planes to the internal layers.

5. Ensure the high-current paths at PGND and VIN have short, direct, and wide traces.

6. SENSE+ and SENSE - are differential pair, make the sense lines run close together, require close parallel and equal length routing. The purpose is to reduce the line drop error.





TYPICAL APPLICATION CIRCUITS





TAPE AND REEL INFORMATION

Package	Carrier Tape	Reel	Reel Color	Pin1	Qty/Reel	Reel / Inner Box	Inner Box / Outer Box	Qty/Out Box
QFN-20	W=12 P=4	13inch	Blue	Q1	5000	1	8	40000
TSSOP20-EP	W=12 P=4	13inch	Blue	Q1	4000	2	8	64000

0

Q2

0 Q1

Q3 Q4

0 0 0 0

PACKAGE INFORMATION





Symbol	Dimensi	ons In Mil	limeters	Dimensions In Inches			
Symbol	Min.	Nom.	Max.	Min.	Nom.	Max.	
А	0.70	0.75	0.8	0.028	0.030	0.031	
A1		0.02	0.05		0.001	0.002	
A2		0.55			0.022		
A3		0.203REF		(0.008REF	=	
A4	0.075		0.18	0.003		0.007	
b	0.2	0.25	0.3	0.008	0.010	0.012	
D		3BSC		O	.118 BS(C	
E		4BSC		0.157 BSC			
е		0.5BSC		0.020BSC			
L	0.3	0.4	0.5	0.012	0.016	0.020	
D2	1.6	1.7	1.8	0.063	0.067	0.071	
E2	2.6	2.7	2.8	0.102	0.106	0.110	
Д	0.01		0.09	0.0004		0.0035	
к		0.25REF		0.	0098 RE	F	
aaa		0.1			0.004		
bbb	0.1				0.004		
ссс	0.1			0.004			
eee		0.08			0.003		
fff		0.1			0.004		

SIDE VIEW



TSSOP20-EP



	Symbol	Dimensions In Millimeters		Dimensions In Inches	
		Min.	Max.	Min.	Max.
	D	6.4	6.6	0.252	0.259
	D1	4.1	4.3	0.165	0.169
	ш	4.3	4.5	0.169	0.177
	b	0.19	0.3	0.007	0.012
	Ċ	0.09	0.2	0.004	0.008
	E1	6.25	6.55	0.246	0.258
	E2	2.9	3.1	0.114	0.122
	А		1.1		0.043
	A2	0.8	1.0	0.031	0.039
	A1	0.02	0.15	0.001	0.006
	e	0.65(BSC)		0.026(BSC)	
	L	0.5	0.7	0.02	0.028
	Н	0.25(TYP)		0.01(TYP)	
	θ	1°	7°	1°	7°

	$\boldsymbol{\mathcal{A}}$
C	\checkmark
1	



REVISION HISTORY

Revision	Data	Description
1.0	2024-05-06	Initial Release

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